

# High Performance Brushless Direct Current Motor Speed Regulator

**Maheswaran Shenthuran and Shanavas Moosafintavida\***

*Azteca University, Mexico, North America*

\*Corresponding author: shanavas.musafi@gmail.com

**Received:** 02-10-2021

**Revised:** 28-11-2021

**Accepted:** 01-12-2021

## ABSTRACT

A robust Fractional-Order Sliding Mode Controller [FOSMC] to control the speed of the D.C. motor. It is computer software and simulation-based research. D.C. motors are one of the most versatile electric machines widely used in industries and home automation. Many control techniques have been proposed to effectively control the position and speed for industrial and domestic purposes. Research activities are focused on developing new techniques for fractional-order controllers as an extension of modern classical theory. Fractional order control is an emerging area of research; this research presents a novel fractional order sliding mode controller for the D.C. motor's speed control. The system is subjected to parametric uncertainties and un-modelled dynamics. Fractional order sliding manifold is defined based on fractional calculus, and stability of the system is guaranteed using Lyapunov theorem. Simulations to be carried out in MATLAB Simulink and simulation results are verified through experiments. The desirable and superior performance of the proposed control scheme to be observed from simulation and experimental results.

**Keywords:** D.C. motor, FOSMC, speed control, BLDC, motor speed regulator

Speed motor drives are used in different sectors for different purposes. They are used in domestic, commercial, and industrial functions as well<sup>[1]</sup>. Despite being expensive, DC [Direct Current] motors, in the past, have been used greatly in all the above-mentioned areas. When compared to an induction motor, the power inverter and control principles are simpler in DC brushed drives. The reason for this being the approximate proportionality between armature current and torque. Also, the speed and armature voltage

**How to cite this article:** Shenthuran, M. and Moosafintavida, S. (2021). High Performance Brushless Direct Current Motor Speed Regulator. *IJISC*, 08(02): 79-92.

**Source of Support:** None; **Conflict of Interest:** None



are related<sup>[2,3]</sup>. While there are some advantages of a DC brush motor, it also has some disadvantages. Some of the main advantages include, but are not limited to the following<sup>[4]</sup>:

- ❖ High principal cost
- ❖ Constant maintenance of commutators
- ❖ Substitution of brushes
- ❖ DC motors cannot be used in clean environments

To remove the high principal cost, the traditional DC motors can be replaced with squirrel cage induction motor; however, some disadvantages are also associated with the induction motor. The major disadvantages being the low power factor and low starting torque<sup>[5]</sup>. There are, however, certain cases where neither a DC motor, nor an induction motor can be used. In such cases BLDC motors are preferred. BLDC motor is most efficient motor for different purposes<sup>[6]</sup>. When compared to a traditional electric motor, a brushless DC motor has several advantages. Some of the advantages are given below:

- ❖ Better torque
- ❖ Increased efficiency
- ❖ Greater dynamic response
- ❖ No brushed involved hence less maintenance
- ❖ Less rotor inertia

To achieve current commutation in a brushless motor, solid-state switches are used. The brushless DC motors are driven by direct current voltage and its working is like the synchronous motor of a permanent magnet. To determine the rotor position for the commutation, position sensors or techniques which do not need a sensor are used<sup>[7]</sup>. Just like the traditional DC motor, the brushless DC motor is also used in different sectors for different purposes. Some of the uses included Steel spinning crushers, electric lines, electric locomotive, air travel, and automation<sup>[8]</sup>. All the applications of a brushless DC motor can be divided into two types [depending on the type of load] namely: Constant & Varying loads<sup>[9]</sup>.

**Application with constant loads:** In such appliances, the capacity is promptly linked with the motor pipe. Some of the examples of a constant load are fans, blowers, and pumps. In all the above-mentioned applications, the speed varies instead of being kept constant at a set-speed. These applications operate in open loop system and have low-cost controllers<sup>[10]</sup>.

**Applications with varying loads:** Some of the main examples of this type of applications include washers, dryers, and compressors. These applications are also used greatly in the automotive and the aerospace industry [Centrifuges, pumps, robotic arm control]. They demand high speed control precision and strong dynamic response. For such application the load varies with the motor across a broad range of speeds<sup>[11,12]</sup>. In contrast with the constant load application, these applications use close-loop systems and use speed feedback devices. The price of such system is higher compared to constant load applications as they use advanced control systems<sup>[13]</sup>.

**Objective:** The aim of this research is to design and apply an advanced control technique that will be used in a high-performing brushless DC motor. Despite the presence of external hindrances, the controller aim is to achieve a decent speed control. To obtain the above aim, the first step was used to find the correct

PID controller parameter. For this purpose, the GA optimization technique was used. In the second step, the self-adjusting fuzzy PID controller is used to design an advanced control system. In the third step, the MRAC technique is utilized. In the final stage, the MRAC technique was used along with the PID compensator. This is one of the latest control techniques.

**Background of the study:** To achieve an efficient drive system, it is essential to achieve advanced control techniques. In most of the industrial functions such as steel spinning grinders and locomotive, an efficient variable speed motor drive system that performs well is of utmost importance. In all the above-mentioned applications [and even more], a PID controller is used greatly because of its advantages i.e., simplicity, toughness, and relaxed tuning parameters<sup>[14]</sup>. A traditional PID control, however, has two drawbacks. The first drawback in the above is the parameter collection, where some of the techniques being used fail to reach the correct PID controller parameter. Techniques like genetic PID tuned controller has been used in different research studies as well<sup>[15]</sup>. Other research studies<sup>[16]</sup> have used PSO and BF techniques in brushless DC motors. Besides,<sup>[17]</sup> used swarm optimization technique for brushless DC motor<sup>[18]</sup> explained the usage of GA-based PIC controller for a brushless DC motor. Just like the above, the use of sensible procedures has been shown in modification of a PID device.

As mentioned earlier, the above applications are faced with external disturbances and variations. This gives rise to the second major problem associated with the conventional PID controls which is fixed parameters. To minimize the effects of this problem, advanced control technology must be used. Different research has been conducted keeping in mind the above-mentioned problem. One study compared a fuzzy Proportional Integral Derivative [PID] controller with a conventional Proportional Integral Derivative [PID]<sup>[19, 20, 21]</sup>. Another study discussion of the development of the fuzzy PID controller<sup>[22]</sup>. Another study used virtual instruments in the implementation of fuzzy logic-based sensor less control<sup>[23, 24]</sup>. Hybrid fuzzy PI controller for speed control has also been implemented in<sup>[25]</sup>. Another method has also been illustrated in<sup>[26, 27, 28]</sup>, where model fuzzy self-tuning of Proportional Integral Derivative device for chopper Fed Direct Current engine force is utilized.

Other studies have discussed different models as well like the use of a modified model reference adaptive controller<sup>[29, 30]</sup>. Other models investigated the effects of fuzzy system of MRAC<sup>[31]</sup>. Model reference adaptive control has also been used<sup>[30]</sup>.

**BLDC motor mathematical model:** To study and analyse the behaviour of a brushless DC motor, it is important to build mathematical models. BLDC motor has three parts in general namely: engine configuration, energy steering path and position device<sup>[24]</sup>. When designing a brushless DC motor, the most crucial part is the removal of the mechanical commutator and its replacement with an electric switch circuit<sup>[32, 19]</sup>. When using an old DC motor, the scrapes are utilized for commutation, this makes the direction of the armature magnetic field perpendicular to the main magnetic field<sup>[33, 16]</sup>. The designing and working principle of a BLDC motor is remarkably similar to brushed Direct Current motor. It has the rotor and the stator. Stator has been made from laminated steel, which is grouped together to carry the windings. In general, there are two ways of arranging a stator namely: the star arrangement and the delta arrangement. The only distinction amongst the arrangements is the amount of torque. While the star pattern is known for giving excessive force at small RPM, the star arrangement delivers minimal force at minimal RPM<sup>[34, 35]</sup>. To get higher torque in a brushless DC motor, the number of poles is increased.

The brushless DC motor has two major types: sinusoidal and trapezoidal. In sinusoidal motor the induced back EMF has sinusoidal form and require sinusoidal-phase current to operate without torque

undulation. On the other hand, the trapezoidal type has a trapezoidal shape of the induced back EMF. To get ripple-free torque operation in trapezoidal type, quasi-square current must be supplied<sup>[29]</sup>. The sinusoidal type is slightly more complex than the trapezoidal type as it requires high resolution position sensors. It also needs complex hardware and software systems<sup>[17]</sup>. Owing to its simplicity and lower price, the trapezoidal type is preferred for industrial applications<sup>[1]</sup>. Besides, a decent amount of precise control hardware [electronic devices] and software are used in the trapezoidal motor<sup>[26]</sup>. This mathematical model is mainly deals with the trapezoidal motor, a transverse section of a brushless direct-current motor. To find the small magnets attached to the brushless DC motor, hall-effect sensors were used<sup>[23]</sup>. A brushless DC motor has three phases but operates based on two phases only. One phase is closed, while the other two with maximum torque are used. The rotor position plays an important role and the three-digit number produced by position sensors change every 60 electrical degrees<sup>[29],[31]</sup>.

A cross-section of three-stage star-associated engine highlights the phase energizing sequence<sup>[25]</sup>. At the start, the rotor and the stator field lines are 120 electrical degrees apart and come to 60 electrical degrees at the end. At 90 electrical degrees, when the field lines are perpendicular, maximum torque is achieved<sup>[21]</sup>. The current commutation that is done by six-step inverters with the switching sequence that directs to the current and the position sensor signal.

**Mathematical model:** Three different equations are coupled together to form a model equation of a brushless DC motor. The three equations are voltage equation, torque equation and motion equation. Just like an induction motor, the stator of a brushless DC motor has three windings<sup>[1]</sup>. The two mathematical models will be discussed namely: transfer function and state space model with the equations given are centred around:

- ❖ Stator having Y connected focused fully field windings.
- ❖ Internal rotor with no salient rod formations.
- ❖ Three hallway devices at 120 electronic degree intervals.

**Transfer function model:** Research conducted had concluded that transfer functions are mostly used in the field of signal processing, communication, and control theory<sup>[22]</sup>. This type of model is used in systems which comprises of a solo-input and solo-output filters. Most of the operating systems work non-linearly; however, when these systems are operated as per the nominal parameters, they resemble LTI [linear, time-invariant system] in their operation<sup>[21]</sup>.

The following assumptions were made while working on the transfer function model in the research<sup>[1]</sup>:

- ❖ Ignore the eddy current losses.
- ❖ Ignore the armature reaction.
- ❖ Ignore the cogging effect.
- ❖ Ideal features of switches involved [power switches].

The working mechanism of a back-EMF is like that in brushed DC motor; therefore, a similar analysis method was used for a three-phase brushless DC motor circuit and a simplified circuit where two phases are working at any given time. If ignored, the electromagnetic time constant and the armature inductance becomes 0.

**State space model:** Due to the development in computer techniques, the State Space Model has become well-known. All computer control systems [including the Kalman filters and dynamic system identification] are centred on state space models.

**Control techniques:** These techniques will be used to achieve high performance control techniques.

**GA-based PID controller:** This method is used in different engineering fields due to its simplicity and reliability. The transfer function of this method is given by:  $[s] = KP + Ki/s + Kds$

In the above equation:

$Kp$  = Proportional gains

$Ki$  = Integral gains

$Kd$  = Differential gain

The role of the proportional gain is to lower the error answer, the role of integral part is eliminating the constant-state inaccuracy, and the role of differential gain is to dampen the dynamic response. It also plays an important role in improving the system stability<sup>[21]</sup>. The most-common method of finding the correct PID control parameter is Ziegler-Nicholas rule<sup>[27]</sup>. The plant parameter is first found by using a step-input. The TI, K, TD plant settings are derived from the phase experiment. The parameters concluded from the Ziegler-Nichols rule might not always give the best-possible results. In such cases, other rules or techniques should be preferred. Some of the techniques that can be used instead of Ziegler-Nichols's rule include Genetic Algorithm, Particle Swarm Optimization and Ant Colony Optimization. Such methods will result in better performance than the Ziegler-Nichols rule<sup>[16]</sup>.

Genetic Algorithm [GA] technique is used widely in engineering and scientific field. For this research as well, GA has been utilized to tune the PID device limits. For this purpose, three different cost functions have been used. The GA toolbox in MATLAB was also used for simulation. To get efficient results, higher number of chromosomes are required. For this purpose, the encoding of the GA chromosomes was conducted. After that, the population was constructed. In the research, 80 chromosomes have been used keeping in mind the execution time<sup>[25],[28]</sup>. Each gene consists of three considerations i.e.,  $Kp$ ,  $Ki$ , and  $Kd$ . For better results, the initial values were obtained from the Ziegler-Nichols rule.  $80 * 40$  matrix was used to represent the population in each generation. In the equation below,  $n$  represents the number of chromosomes. Each row in the above equation represents one chromosome. The fitness value  $[f]$  of the chromosome<sup>[15],[17]</sup>. Several cost function can be used to find the value of  $Kp$ ,  $Ki$ , and  $Kd$ . In this research, three different cost function have been used.

**First cost functions:** The composition of GA tuning method for the first-cost function. Error signal is the only input for the GA tuning system, which, in most cases, does not give accurate or efficient results. While the first cost function is known for improving the overall performance, it does not necessarily give a decent rise time and satisfactory overshoot.

**Second Cost Functions:** Just like first cost function, there are some problems associated with the second cost functions. Second cost functions are used to improve the overall performance of systems; however, there is an inverted connection amongst rise time and overshoot of the locked loop approach. This prevents the system from getting good results<sup>[21]</sup>. In the equation,  $tr$  represents the rise time,  $Mp$  represents the maximum overshoot,  $ts$  represents the settling time and  $ess$  represents the steady state error.  $C1$  to  $C4$  are the weighting factors,  $trd$  is the anticipated elevation time, and  $Mpd$  is an anticipated highest overstep.

**Third cost function:** An advantage of the third cost function is that it can handle the problems that were mentioned for the first and second cost function. By using the weighting factor, this expense event can comply with the designer obligation.

**Self-tuning fuzzy PID controller:** The online modification of the device parameter increases the execution and robustness of the system. Keeping in mind the above-mentioned fact, this study aims at designing a fuzzy PID controller with auto-adjustment. This type of controllers is especially efficient in the cases where high external disturbances are observed<sup>[5]</sup>. The two parts of the controller. The primary portion is the PID device, and the other part is the fuzzy logic controls.

**Fuzzification:** Fuzzification is a technique that is used to transform the feedback statistics into linguistics principles. There are two inputs involved namely: inaccuracy and change in inaccuracy. The linguistic labels for the system at hand gives descriptions are as follows: large negative, medium negative, small negative, zero, small positive, medium positive and large positive.

**Rule Base:** The decision-making process resembles the human decision process. The inputs have 7 different linguistics labels which give us 49 different rule bases. The medium label is ignored, which leaves behind only 25 rule bases.

**Defuzzification:** The motivation behind defuzzification measure is to convert the fluffy yield into fresh worth to practice as a non-fluffy regulator activity. There are a wide range of techniques for defuzzification; however, the defuzzification procedure that has been utilized in this research is demonstrated in equation below. In the equation,  $u[uj]$  is the degree to which the elements of  $uj$  belongs and  $u[nT]$  is an outcome of the fuzzy controls. The alphabet  $n$  represents quantity of the convention standards. In this research author will apply adaptive control method to avoid any disadvantages of self-tuning fuzzy PID control to get high performance from the brushless DC motor.

**Model reference adaptive control:** The Model Reference Adaptive Control [MRAC] is one of the best adaptive control techniques being used today. It also represents an efficient way of specifying the servo problem<sup>[27],[29]</sup>. This technique is regarded as a versatile servo framework in which the ideal execution is communicated as a reference model. This gives the ideal reaction to an order signal.

In general, a MRAC regulator comprises of an orientation model a regulator law and a flexible system which refreshes limitations by utilizing criticism mistake amongst the reference model and the genuine plant. The essential guideline of this flexible regulator to fabricate the reference prototypical which indicates an ideal yield of a regulator and afterward variation law changes the undisclosed boundaries of plants, so the error of tracking is completely minimized<sup>[28]</sup>. Two loops are joined together to make the adaptive controller. While the outer loop plays a crucial role in minimizing the difference between the process and model output, the inner loop comprises of the procedure and common feedback regulator<sup>[29]</sup>. To minimize the loss function, the MIT rule is used in the model-reference adaptive control. This rule was first introduced in MIT's laboratory. In the equation, the adaptation gain is given by  $\gamma$ , the error between the output speed and the model output is given by  $E$ .  $\theta$  represents the controller parameter. A linear regulator with two degrees of self-determination with an equation, the damping ratio is 1, the natural frequency is 500.

**MRAC with PID compensator:** The main purpose of Model Reference Adaptive Controller is to remove the distinction amongst the output of reference model and the genuine speed. While doing the above, it ignores the error concerning the speed of reference and the real speed. It might trigger elevated overshoot

and the elevated settling times. The burden can be eased by embracing to PID compensators. To achieve the highest output and efficient performance, the parameters used for a PID compensator were like that of GA-based PID controller.

**Open loop response result:** By using MATLAB, the simulation of the BLDC motor was carried out. The parameters were used for the MATLAB simulation. By substituting the parameters, the voltage inverter used in it is of six-steps. To decode the hall effect signal, inverter gates signals were used. Similarly, its responses that was obtained by using a brushless DC motor open loop system. The speed becomes constant at 4000 rpm. The speed the  $n$  drops to 3100 rpm when the weight is amplified by 50%. The variance in the current phase of the open loop system is evident from that the current increased to  $\pm 2.5A$  when the load torque is increased. It is evident that at 0 torque, the electromagnetic torque is 0.03N.m and rises to 0.2N.m when the load is increased.

**Result of close loop response:** The techniques were implemented are the results obtained are discussed below:

**GA based PID control:** Four different arrangements of PID boundaries were used for the BLDC engine drive. The initial set was acquired by utilizing Ziegler–Nichol’s rule when the additional three groups are attained by utilizing GA dependent on the three distinctive expense capacities as portrayed in earlier chapters. The scope of progress of PID regulator boundaries through streamlining measure. The parameters that were obtained from the Ziegler-Nichols method for the PID control are the evident for third cost function which has the best performance amongst other techniques.

**Self-tuning fuzzy PID control:** The results obtained in the previous section helped in concluding that the GA built PID regulator with CF3 gives the finest presentation; therefore, the similar initial values were used for the self-tuning fuzzy proportional integral derivative controller. The Simulink outline of the brushless direct current engine drive framework with self-tuning fluffy PID regulator. The regulator comprises of dual fragments, PID regulator and fuzzy logic regulator. Keeping in mind the errors and the change of errors the fuzzy logic regulators are utilized to tune online the PID regulator boundaries.

**Model reference adaptive control with the PID compensators:** In this section the performance of the BLDC engine driver framework utilizing MRAC with the PID compensator has been investigated. Previous results have shown MRAC gets high overshooting & settling time and the impacts of accumulation PID compensator to MRAC at various estimations of variation expansion. Therefore, a quick result with the overshoot is achieved. This implies that expanding the adaptation gain will diminish the ascent time exclusive of expanding the overshoot.

## Control technique performance investigation

**Speed regulation at sudden load:** The capability of the regulator to accomplish the required speed using a contrast of different techniques. The PID have better performances as the overshoot recorded was small and it had less rise time. The routine of each regulator procedure of MRAC with the PID controller gives best routine amongst all procedures conforms regulator output and DC supply current.

**Speed Response at parameter variation:** The changes that occur when the rotor inertia and phase resistance is changes instantly.

**Sudden changes in phase resistance:** When running industrial applications for longer periods of time, the phase resistance often requires some changes in it. In this section, the phase resistance [R] will be reduced by 50% suddenly to test how the proposed control techniques respond to it. This will be done in 0.1 seconds. The MRAC with a PID compensator responded quicker than other procedures. MRAC with the PID compensators are quicker and flexible when it comes to responding to different external disturbances.

**Changes of rotor inertia and phase resistance:** This section will investigate how the control techniques respond when both, rotor inertia and phase resistance, are changed by 20%. The swiftness retort of each regulator procedure when the phase confrontation and rotor inertia were increased by 20% simultaneously leading MRAC and PID compensator to respond better than other techniques. The performance of different control techniques when the R & J were increased by 20%, It is evident from the results that the MRAC with PID compensator has a decent overshoot, fewer rise time and fewer settling time as well.

**Speed regulation at sinusoidal load:** The sinusoidal load on a Brushless DC motor is constantly changed to test the quickness of the proposed control techniques. The motor was unprotected to varying sinusoidal load [between 0 and 50%] of the valued torque to see the speed response of each control technique. The engine swiftness is wavered around orientation speed. Every control method looks to follow the orientation speed. Reference speed is being tracked by the different control techniques that have been used. The maximum percentage of deviation varied between the different control techniques. Efficient performance is achieved when the control technique has a small deviation percentage. It is also noted the online tuning methods will provide better performances for control techniques. The maximum deviation of each control technique obtained the MRAC with the PID compensators owns bottom extreme eccentricity about the speed of the references.

**Speed tracking:** The control techniques used in the research respond to the different speeds. The use of varying speeds is a common practice in assembly lines.

**Diverse guidelines of orientation speed:** The control techniques responded to the commands of different speeds. The MRAC with the PID compensators had quickest response to reference speed with the output of the respective controller and direct current power supply for each technique. It changes reference speed commands, the DC supply current increases.

**Trapezoidal speed tracking:** A key feature of a trapezoidal speed tracking system is that it changes speed linearly. When increasing or decreasing speed, it changes linearly. The speed vs time, the model reference has bad performance at the start. Furthermore, it may also be noticed that GA based proportional integral derivatives controllers have high deflection speeds when the MRAC with the proportional integral derivatives compensators and self-setting PID regulators having a minor non-conformity. Therefore, it conforms control output and DC supply current with respect to the trapezoidal speed tracking.

**Laboratory set-up and test findings:** The practical implementation of the control techniques setup of the brushless DC motor The System identification of toolbox in MATLAB will also be utilized in this section to setup an estimated transmission function for the brushless DC motorized drive arrangement.

**Workshop arrangement:** The main components of the brushless motor drive system comprise of 6 power transistor, MOSFET inverters, drive circuits and the three halls effective devices.

Following is a detailed description of the experimental set-up:

- ❖ A 50-watt Maxon brushless DC motor was used with three hall effect sensors. The main function of the trio hall effect sensors is to distinguish the rotor location and speed requirement.
- ❖ A 97-watt brushless EC motor that is used for the efficient control of permanent magnet. The servo controller that was used is ESCON 36/3 which is 4-quadrant PWM servo controller.
- ❖ An input of 220V and 6A with an output of 24V.
- ❖ The control algorithm was performed by using a computer
- ❖ USB-6008 data acquisition card which has the following specifications:
  - I/O 12 digit
  - 2 analog outputs
  - 8 analog inputs

**Data acquisition in MATLAB:** To transfer the data between the real world and the computer, MATLAB's data acquisition toolbox was used. This was done by using a USB-6008 DAQ device. The statistics attainment tool cabinet offers a various instrument for analogue inlet and outlet. It also offers digital inputs and outputs from different compatible PCs statistics attainment hardware. As mentioned earlier, the role of the tool case is to convert the real-life data into MATLAB data, where a Simulink is created to get fast analysis. Another advantage of using the MATLAB data acquisition toolbox is that it enables the user to incorporate real life data into a Simulink model. The model is then verified and validated against the data input.

**Identification of the system:** Developing a transfer function of nonlinear components is a difficult task. The non-linear components consist of inverter and logic and circuit. The equation represents the approximate transfer function:  $[s]$  represents the rotor speed and  $V_c[s]$  represents the precise voltage of the systems. In the above-mentioned equations a, b and c represents the parameter of the transferring functions. The MATLAB systems identification toolbox was utilized to identify the parameters of approximate transfer function. To progress the second order transfer function of the drive scheme, real time data for the input and output was obtained from the MATLAB data acquisition toolbox.

**Results of open loop response:** The equation below represents the developed transfer function. Similarly, the legitimacy of the identified transfer function which has been used to simulate the brushless DC motor drive system. It is also evident that real brushless DC motor can simulate the developed transfer function by 90%. Nonlinearity in the system is the main cause behind the small difference that can be distinguished between the recognized transfer functions and the motor drive systems of the actual brushless DC motor.

**Closed loop response results:** By using the different types of control techniques, this system explains the experimental results that were obtained from the brushless DC motor drive system.

**GA-built PID control:** Three different sets of parameters were used for the practical implementation of the GA-based PID controller. The parameters were achieved by using the identified transfer function model; therefore, it can be rightly said that the parameters were obtained off-line. The model of GA base proportional integral derivative controller. As mentioned in the previous section as well, Ziegler-Nichols model was used to get the initial set of parameters that was used to achieve the results. To get the other sets of parameters i.e., second, third and fourth set, three different cost functions were used with respect to GA.

The four sets of controller parameters sets were obtained by using the Ziegler-Nichols rule and the GA technique with respect to the three different cost functions. To find which set of parameter gives the best output and efficient performance, each set of controller parameter was applied on the brushless DC motor drive system. The simulations consequences of the four PID controllers that were functional on the T.F. model. The GA-built PID controllers [CF1] have similar performance as the Ziegler-Nichols technique. Both the above techniques are centred around minimizing the error. When compared to other methods, GA-built PID regulators [CF-3] have finest recital. GA-based PID controller had the most efficient performance amongst others. It had the minimum rise and settling time and had almost 0 overshoot.

The experimental results that were obtained from the real system when the four PID controllers were applied on it and the experimental results are similar. The GA-based PID controller [CF3] had the most efficient performance amongst others. The performance of different sets of PID controllers had the minimum rise time and settling time. Due to this reason, the GA-based PID controller is better than other methods. By comparing, we can see differences in the simulation results due to the non-linearity and the signal noise.

**Self-tuning fuzzy proportional integral derivative controllers:** A key feature of the fuzzy control PID is that it can adjust the PID control parameters with the error and change in error that occurs during the application or experiment being performed. To achieve good results, this research used the initial constraints of the GA-built PID regulator [CF3]. CF3 gave decent consequences that have been discussed extensively in the previous section; therefore, the same parameters were used once again to achieve decent results. The Simulink of practical self-tuning fuzzy Proportional Integral Derivatives Controllers have the speed retort of the brushless DC motors drive scheme utilizing self-tuning fuzzy Proportional Integral Derivative Controller.

**Model reference adaptive controller:** The speed reaction of a brushless motor drive systems has been demonstrated by using Model Reference Adaptive Control [MRAC]. In this technique, the focus is on getting similar outputs in the actual plant track and reference model. TO achieve the above, the similar reference inputs are used. MRAC performed for different values of adaptation gains when the adaptation was increased, it in return increased the overshoot and decreased the rise time.

**Model reference adaptive controller with PID compensators:** The consequence of adding PID compensator to Model Reference Adaptive Control [MRAC]. The rise time decreases without increasing the overshoot when the adaptation gain is increased. The parameters used for the proportional integral derivative controller is similar as the GA built proportional integral derivative controller [CF-3]. Once again, the reason for using similar parameters is the efficient performance that was achieved from CF3 in the previous sections. A Model References Adaptive Control with proportional integral derivative controller compensators performed at the identified adaptation gains. As the adaptation gain increases, the rise time decreases [it gives faster response] and increases the arrangement exceed

## Control techniques performance investigation

**Speed regulation test:** To find an efficient control technique, this section explains in-depth the comparison between different control techniques that have been addressed throughout the research. The rotor speed has been plotted against the time. The self-tuning fuzzy proportional integral derivative controllers has improved performance than the GA-built proportional integral derivative controller. Recital of Model

Reference Adaptive Control is improved than the self-tuning fuzzy PID regulator; however, it aches from an extreme overshoot and elevated settling time. When MRAC is used with the proportional integral derivative compensators, it will be able to minimize the disadvantages of MRACs. The experimental results obtained are in line with the theoretical results that were identified in the previous section. Therefore, it summarized the recital of all controller procedure. MRAC has the minimum rise amongst other techniques; however, it has elevated overshooting and extreme settling time. These drawbacks, however, can be minimized by coupling MRACs with a proportional integral derivative compensator where it has a decent elevated times and overshoot.

**Speed tracking test:** When investigating industrial applications, it can be concluded that some applications require a constant speed, while the others require a constantly changing speed. The investigational consequences of a test will be communicated which will prove how the different regulator procedures performed at diverse instructions of reference speed. The speed responded for the three various controls procedures at diverse instructions of the referenced speeds. The test was conducted on all the techniques that have been studied in detail throughout the experiment. The test results helped in concluding that the MRAC has a better [faster] response amongst all the techniques. Other techniques that were used in the research include GA proportional integral derivative control and the self-tuning fuzzy proportional integral derivative controls; however, a drawback is, once again, associated with the above which is that it aches from a high overshoot and extreme settling time. The effects that result when PID is coupled with a Model Reference Adaptive Control. When a MRAC was coupled with PID and used, it resulted in a faster response and a minimal overshooting time.

## CONCLUSIONS & RECOMMENDATIONS

As mentioned in the introduction section of this research the Brushless Direct Current [BLDC] motors are used widely for the different industrial applications. Main aim of this research was to obtain a brushless DC motor which performs exceptionally well and minimizes the drawbacks that are widely prevalent in a PID controller. A major problem in this was the selection of the parameters. This problem was addressed efficiently in this research, where the Genetic Algorithm [GA] optimization procedure was utilized to find the correct regulator limitations keeping in mind the trio diverse cost functions. Different simulations and experiments were conducted which helped in concluding that the GA built on third cost function attained the efficient presentation amongst all extra cost functions involved.

Another major delinquent that is widely prevalent in the orthodox PID control is that it has static limits which are not appropriate for all the working circumstances. Similarly, it is unable to deal with peripheral conflicts efficiently. Keeping in mind the above, this research aimed at designing and implementing three different advanced control techniques to minimize the problems mentioned above. This first technique used was the self-tuning fuzzy proportional integral derivative control where the tasks of the fuzzy controls was to adapt to the PID parameters keeping in mind the errors and the change in errors. This was done to ensure that the necessary speed was monitored. Second method of investigation was the MRAC where the expected return is expressed according to the reference model. As reflected in the results and discussion section, the MRAC has quick responses; however, it aches from an elevated overshoot and extreme settling time. The third technique that was used in the research is the MRAC with PID compensator. An advantage of the modifiedMRAC is that it minimizes the drawbacks that are widely prevalent in the normal MRAC [high overshoot & high settling time]. When using a modified MRAC, a fast response is

achieved with the high overshoot. The simulation conducted and the investigational consequences were similar which help in concluding that the modified Model Reference Adaptive Control with Proportional Integral Derivative controller is more efficient than the other procedures involved.

To conclude the research, it can be rightly remarked that the research helped in identifying a new methodology that can be used to obtain the current parameters. This was done by using the GA optimization procedures are three various costs functions were used to accomplish high performing brushless DC motor drive systems. Secondly, the research also aided in improving the system recital by consuming the fuzzy logic controls technique that has been utilized to tune the proportional integral derivative controller regulator parameter. This was done with respect to the error and change of errors. Thirdly, the results obtained from the experiments and Simulink also helped in concluding that the Model Reference Adaptive Control [MRAC] achieves efficient performance as analysed to the GA based proportional integral derivative controller and self-tuning fuzzy proportional integral derivative control; however, a drawback was also identified. The MRAC also griev from an elevated overshoot and an elevated settling period. Similarly, the research identified a major conclusion where a new technique has been identified. This technique used the MRAC with a PID compensator. The initial parameters used in the modified MRAC were like GA-based PID controller [CF3]. Similarly, by using MATLAB system identification toolbox, an estimated transfer function to BLDC motor drive system was developed. Lastly, this research aided in applied application of four innovative monitoring methodologies are applied to the laboratory set-up of brushless DC motor drive systems. This was done to highlight about which system achieved the highest performance.

## Future work

For future investigations on a similar topic, it is recommended that new optimization techniques should be used to tune proportional integral derivative controller settings such particle swarm optimization and ant colony optimization methodologies. These techniques might help in identifying better PID regulator limitations and hence improved recital of the brushless DC motor drive system. Similarly, it is recommended to the study the effect of accumulation Fractional Order Proportional Integral Derivative controller compensators to a Model References Adaptive Control as an alternative of a proportional integral derivative controller compensators.

## REFERENCES

1. Qu, L., Hu, H. and Huang, Y. 2010. Fractional order P.I.D. controller based on particle swarm optimization implemented with FPGA, in: Proceedings of the International Conference on Artificial Intelligence and Computational Intelligence [AICI-2010], IEEE Computer Society, 23–24, pp. 165–169.
2. Hung, J.Y., Gao, W. and Hung, J.C. 1993. “Variable Structure Control: A Survey”, *IEEE Trans. on Industrial Electronics*, **40**(1).
3. Shafiei, S.E. 2010. Sliding mode control of robot manipulators via intelligent approaches. In: Shafiei SE, editor. *Advanced Strategies for Robot Manipulators*. Rijeka: IntechOpen, pp. 135-172. DOI: 10.5772/10193.

4. Yu, X and Kaynak, O. 2009. Sliding-mode control with soft computing: A survey. *IEEE Transactions on Industrial Electronics*, **56**(9): 3275-3285.
5. Velagic, J. and Galijasevic, A. 2009. Design of fuzzy logic control of permanent magnet D.C. motor under real constraints and disturbances. *Proceedings of International Conference on Control Applications & Intelligent Control*, pp. 461-466.
6. Kumar, U. and Dohera, D. 2015. Separately excited D.C. motor speed control of using various tuning conventional controllers. *International Research Journal of Engineering and Technology*, **2**(8).
7. Jin, Y., Luo, Y., Wang, C. and Chen, Y. 2009. LabVIEW based experimental validation of fractional order motion controllers, Chinese Control and Decision Conference [CCDC 2009], pp. 323–328
8. Luo, Y. and Quan Chen, Y. 2011. Pi, Experimental study of fractional order proportional derivative controller synthesis for fractional order systems, *Mechatronics* **21**: 204–214.
9. Ruszewski, A. and Sobolewski, 2012. Comparative studies of control systems with fractional controllers, *Przeglad Elektrotechniczny, Electr. Rev.*, pp. 204–208.
10. Kaneda, Y., Sadahiro, T. and Yamakita, M. 2011. FPGA Implementation of digital differentiator using Richardson extrapolation and high sampling rate acting like fractional delay, SICE Annual Conference, Waseda University, Tokyo, Japan, September 13–18, pp. 2378–2383.
11. Podlubny, I. 1999. Fractional-order systems and PI D $\lambda$   $\mu$  controllers. *IEEE Transactions on Automatic Control*, **44**: 208–214.
12. Monje, C.A., Vinagre, B.M., Chen, Y.Q., Feliu, V., Lanusse, P. and Sabatier, J. 2004. Proposals for fractional PI D $\lambda$   $\mu$  tuning. In 1<sup>st</sup> IFAC workshop on fractional derivatives and applications, Bordeaux, France. 1<sup>st</sup> IFAC workshop on fractional derivatives and applications, Bordeaux, France.
13. Domingues, J., Valerio, D. and da Costa, J.S. 2009. Rulebased fractional control of an irrigation canal. In Proceedings 35<sup>th</sup> annual conference of IEEE industrial electronics IECON '09, pp. 1712–1717.
14. Changmao, Q., Naiming, Q. and Zhiguo, S. 2010. Fractional P.I.D. controller design of hypersonic flight vehicle. In international conference on computer, mechatronics, control, and electronic engineering [CMCE], pp. 466–469.
15. Fan, H., Sun, Y. and Zhang, X. 2007. Research on fractional order controller in servo press control system. In International Conference on Mechatronics and Automation, ICMA, pp. 2934 –2938.
16. Bouafoura, M.K. and Braiek, N.B. 2010. PI D $\lambda$   $\mu$  controller design for integer and fractional plants using piecewise orthogonal functions. *Communications in Nonlinear Science and Numerical Simulation*, **15**: 1267– 1278.
17. Podlubny, I. 1999. Fractional-order systems and PI D $\lambda$   $\mu$  controllers. *IEEE Transactions on Automatic Control*, **44**: 208–214.
18. Valério, D. and da Costa, J.S. 2006. Tuning of fractional P.I.D. controllers with Ziegler– Nichols-type rules. *Signal Processing*, **86**: 2771–2784. Special Section: Fractional Calculus Applications in Signals and Systems.

19. Zamani, M., Karimi-Ghartemani, M., Sadati, N. and Parniani, M. 2009. Design of a fractional order P.I.D. controller for an A.V.R. using particle swarm optimization. *Control Engineering Practice: Vol. 17*. In Special Section: The 2007 IFAC symposium on advances in automotive control, pp. 1380–1387.
20. Lee, C.H. and Chang, F.K. 2010. Fractional-order P.I.D. controller optimization via improved electromagnetism-like algorithm. *Expert Systems with Applications*, **37**: 8871–8878.
21. Cervera, J., Banos, A., Monje, C. and Vinagre, B. 2006. Tuning of fractional P.I.D. controllers by using QFT. In 32<sup>nd</sup> annual conference on IEEE industrial electronics, IECON, pp. 5402–5407.
22. Utkin, V.I. 1977. Variable structure systems with sliding modes. *IEEE Transactions on Automatic Control*, **22**(2): 212-222.
23. Bengiamin, N.N. and Kauffinann, B. 1984. “Variable structure position control,” *IEEE Trans., Control System Magazine*, **4**(3): 3-8.
24. Chan, W.C. and Hsu, Y.Y. 1981. Automatic generation control of interconnected power system using variable-structure controllers. *I.E.E. proc, C, Gen. Trans. & Distrib.*, **128**(5): 269-279.
25. Bengiamin, N.N. and Chan, W.C. 1982. “Variable structure control of electric power generation,” *IEEE Trans., PAS-101*, pp. 376-380.
26. Edwards, C. and Spurgeon, S.K. 1998. Compensator based output feedback sliding mode controller design. *Int. J. Contr.*, **71**: 601-614.
27. Jiang, J. 2007. Sliding-mode variable structure control for the position tracking servo system WSEAS *Transactions on Systems*, **6**(2): 294-297.
28. Wang, S., Habibi, S. and Burton, R. 2006. “Sliding mode control for a model of an electrohydraulic actuator system with discontinuous non-linear friction”, The Proceedings of 2006 American Control Conference, Minneapolis, Minnesota U.S.A., pp. 5898-5904.
29. Harifi, A., Aghagolzadeh, A., Alizadeh, G. and Sadeghi, M. 2005. “Designing a sliding mode controller for antilock brake system”, *Int. Conference on Computer as a Tool, Serbia and Montenegro*, pp. 611-616.
30. Sadati, N. and Ghadami, R. 2008. “Adaptive multi-model sliding mode control of robotic manipulators using soft computing,” *Neurocomputing*, **71**(2): 27022710.
31. Wai, R. and Chang, L. 2006. Adaptive stabilizing and tracking control for a non-linear inverted-pendulum system via sliding-mode technique. *IEEE Trans. Ind. Electron.*, **53**: 674692.
32. Liang, H. and Chong, K.T. 2006. “Variable parameter sliding controller design for vehicle brake with wheel slip,” *J. Mech. Sci. Technol*, **20**(11): 18011812.
33. Xie, W.F. 2007. “Sliding-mode-observer-based adaptive control for servo actuator with friction,” *IEEE Trans. Ind. Electron.*, **54**(3): 1517-1527.
34. Utkin, V.I. 1977. Variable Structure systems with Sliding Modes. *IEEE Transaction on Automatic Control*, **22**(2): 212-222.
35. Raymond A. DeCarlo, Stanislaw H. Zak, and Gregory Mathews, 1988. “Variable Structure Control of Nonlinear Multivariable Systems: A Tutorial”, *Proceedings of the IEEE*, **76**(3).